Plasma-catalytic Oxidation of Toluene on Ag Modified FeO\(_x\)/SBA-15

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**ABSTRACT**

Catalysts created by loading FeO\(_x\) and AgO\(_x\) on SBA-15 surfaces via wet impregnation were used to remove toluene with the assistance of non-thermal plasma (NTP). The catalysts were characterized with X-ray diffraction (XRD), scanning electron microscopy (SEM), and H\(_2\) temperature-programmed reduction (H\(_2\)-TPR). The results showed that incorporating the SBA-15, 3%FeO\(_x\)/SBA-15 and 2%FeO\(_x\)-1%AgO\(_x\)/SBA-15 catalysts enhanced the toluene removal efficiency and CO\(_2\) selectivity of the NTP system. The silver particles tended to cover the catalyst surface in the form of Ag and Ag\(_2\)O, which lengthened the residual time of toluene in the NTP-catalytic system, thereby promoting the reaction of toluene with oxygen on the catalyst surface. Simultaneously, introducing Ag improved the distribution of FeO\(_x\) on the catalyst surface, increasing toluene oxidation and catalyst stability. According to our analysis of the toluene removal efficiency, identification of organic byproducts, and in situ FT-IR spectroscopy of the toluene adsorption, FeO\(_x\) and AgO\(_x\) significantly enhance the efficiency of toluene degradation in plasma-assisted catalytic systems.

**Keywords:** FeO\(_x\)-AgO\(_x\)/SBA-15 catalyst; Toluene removal; Plasma-catalytic oxidation.

**INTRODUCTION**

Non-thermal plasma (NTP) combined catalysis technology is a promising method for VOCs oxidation due to its high economy and energy efficiency (Stasiulaitiene et al., 2016; Lu et al., 2019). At the same time, the FeO\(_x\) shows the outstanding performance for toluene removal in the NTP system. However, CO and other byproducts are formed during toluene degradation, and CO\(_2\) selectivity is low (Lu et al., 2015). In order to overcome these disadvantages, the catalysts of bimetallic materials have been applied for VOCs degradation due to their prominent catalytic activity (Jiang et al., 2016; Zhu et al., 2016; Jiang et al., 2019). Noble-metal-based catalysts, such as Pt, Au, are traditional catalysts for the VOCs oxidation at low temperatures (Li et al., 2016; Yang et al., 2016). However, these pure noble metal catalysts also have some disadvantages, especially their high cost. Scirè et al. (2001) report that Ag could weaken the Fe-O bond, increase the mobility of the lattice oxygen, and thus improve the VOCs oxidation. Meanwhile, Ag has exceptional activity and is more economical (Jiang et al., 2016; Pangilinan et al., 2016). In addition, Ag could work as an adsorption center, improving adsorption ability and oxidation for VOCs (Chen et al., 2011; Huang et al., 2015). However, there has been little research in regards to combining this bimetallic oxide catalyst with NTP for VOCs degradation in the present literatures. Besides that, the effect of bimetallic catalyst on VOCs degradation in NTP system is still not clear. Therefore, we incorporated Ag into the FeO\(_x\) catalyst on account of the characteristics of these two materials, and co-loaded them on the surface of SBA-15 which has uniform mesoporous channels, high specific surface area, and high adsorption ability for toluene (Zhang et al., 2012b; Qin et al., 2019).

In this work, toluene was selected as the targeted pollutant, and the plasma-catalytic oxidization was carried out at identical specific energy density (SIE) under the condition of atmospheric pressure and room temperature. In order to study the structure and possible interaction between FeO\(_x\) and AgO\(_x\) species, the catalysts were characterized by XRD, SEM and H\(_2\)-TPR. In situ FT-IR spectroscopy of toluene adsorption and organic byproducts on catalyst surface were also identified to acquire the toluene oxidation mechanism on the surface of FeO\(_x\)-AgO\(_x\)/SBA-15 catalyst.

**EXPERIMENT**

**Experimental Setup**

The schematic diagram of the experimental setup is
shown in Fig. 1. The toluene was obtained by bubbling liquid toluene with an N\textsubscript{2} gas stream in a bubbler, which was described in our previous study (Lu et al., 2015). Then, the reaction gas was introduced into the reactor with an initial toluene concentration of 100 ppm at a flow rate of 180 mL min\textsuperscript{−1}. The initial toluene concentration and the gas flow rate were adjusted by mass flow controllers (MFCs) (Seven Star Co., China).

Toluene oxidation was carried out in a fixed-bed flow reactor containing 0.12 g of the catalyst (40–60 mesh) and 0.96 g of silica sand (40–60 mesh). The outgoing gas was analyzed using an online gas chromatograph (GC2014C; Shimadzu) equipped with two FID detectors: one for organic compounds, featuring a TG-BOND Q column (30 m, 0.32 mm; 60°C), and the other, equipped with a methanizer, for carbon monoxide and carbon dioxide analysis using a 5 Å molecular sieve (2 m, 2 mm) and PoraPLOT Q column (4 m, 2 mm) (60°C). The toluene removal efficiency and CO\textsubscript{2} selectivity were calculated based on the following formulas:

\[
\text{Toluene removal efficiency (\%) } = \frac{C_{in} - C_{out}}{C_{in}} \times 100\% 
\]

\[
\text{CO}_2 \text{ selectivity (\%) } = \frac{C_{CO_2}}{7(C_{in} - C_{out})} \times 100\% 
\]

where \(C_{in}\) and \(C_{out}\) are the inlet and outlet toluene concentrations respectively, \(C_{CO_2}\) is the outlet concentration of CO\textsubscript{2}. All concentrations were measured in ppm, and the data was recorded by an online gas chromatograph when the toluene removal efficiency was stabilized.

**Plasma System**

The reactor was a cylinder reactor of quartz glass, with an inner diameter of 8 mm and wall thickness of 1 mm. The stainless steel wire mesh was wrapped as the ground electrode, and a stainless steel rod (o.d. = 2 mm) was used as the inner electrode, resulting in the discharge length and discharge gap being 18 mm and 3 mm. The reactor was powered by an AC high-voltage power supplying with the frequency of 2 kHz (CTP-2000k; Corona Laboratory, Nanjing, China). In the experiment, the discharge power was measured by the areas of the voltage-charge Lissajous figures, which were acquired by an oscilloscope (TDS1002; Tektronix) (Li et al., 2014).

The specific energy density (SED) was calculated from the following expression:

\[
\text{SED (J L}^{-1}) = \frac{\text{Discharge power (W)}}{\text{Gas flow rate (L s}^{-1})}
\]

**Catalyst Preparation and Characterization**

The catalysts were prepared using wetness impregnation method. Iron nitrate ethanol solution (Fe/SBA-15 = 2% wt. and 3% wt.) was first added to SBA-15 powder, after being stirred at room temperature for 24 h, the solvent was then removed by evaporation at 60°C. The residue was dried at 120°C for 12 h, calcined at 500°C for 4 h. The resulting catalysts were denoted as 2%FeO\textsubscript{x}/SBA-15, 3%FeO\textsubscript{x}/SBA-15, respectively. After that, Ag was loaded on the catalyst of 2%FeO\textsubscript{x}/SBA-15 using a similar process under the same condition with AgNO\textsubscript{3} solutions as precursors (Ag/SBA-15 = 1% wt.). The resulting catalyst was denoted as 2%FeO\textsubscript{x}–1%AgO\textsubscript{y}/SBA-15.

XRD results were collected using a D8 ADVANCE X-ray diffractometer (Bruker, Germany) operated at 40 kV and 40 mA using Ni-filtered Cu K\textalpha\ radiation, the 2\theta ranges were 0.6–5° and 5–90° at a scanning rate of 4° min\textsuperscript{−1}.

SEM microphotographs were collected with an S-3700N electron microscope (Hitachi, Japan) operating at 5.0 kV. H\textsubscript{2}-TPR data was collected by a Micromeritics AutoChem II 2920 instrument. Each catalyst (40 mg) was pretreated at 300°C in the high-purity Ar (30 mL min\textsuperscript{−1}) for 30 min and then cooled to 60°C. Subsequently, the flow of an H\textsubscript{2}-Ar
mixture (10% H₂ by volume) was switched on, and the catalyst was heated to 700°C at a rate of 10°C min⁻¹. The H₂ consumption was monitored by a thermal conductivity detector (TCD).

**In Situ FT-IR Study**

In situ FT-IR spectra was recorded using a Nicolet 6700 spectrometer equipped with a mercury-cadmium-telluride (MCT) detector cooled by liquid nitrogen. The catalyst was pretreated at 300°C in high-purity Ar (100 mL min⁻¹) for 60 min, cooled to room temperature, then toluene–N₂–O₂ mixture (100 ppm toluene, N₂:O₂ = 20%:80%) was introduced into the IR cell. The infrared spectra of toluene adsorption were collected with a resolution of 2 cm⁻¹ and 64 scans in the region of 650–4000 cm⁻¹.

**Identification of Organic Byproducts on the Catalyst Surface**

The organic byproducts on the catalyst surface were extracted by CS₂ solution (chromatographic grade) at the condition of ultrasonic vibration for 120 min. Then filtered with a 0.22 µm filter membrane, and analyzed by a GC–MS (QP2010; Shimadzu) with Rtx-5MS capillary column. The column temperature was firstly maintained at 40°C for 2 min, then increased to 220°C with a rate of 6°C min⁻¹, and maintaining for 5 min. MS identification was conducted using the NIST 08 databank (NIST/EPA/NIH Mass Spectral Library).

**RESULTS AND DISCUSSION**

**Catalytic Activity Evaluation**

The results of toluene removal efficiency and CO₂ selectivity were showed in Fig. 2. The toluene removal efficiency was only 47% under the condition of NTP, while it significantly increased as the various catalysts were packed into the plasma system. The toluene removal efficiency caused by SBA-15, 3%FeOₓ/SBA-15, 2%FeOₓ–1%AgOᵧ/SBA-15 increased by 48.9%, 50.3%, 51.3% respectively. CO₂ selectivity had no significant change over the SBA-15, while it was increased by 11% over the 3%FeOₓ/SBA-15 and 17% over the 2%FeOₓ–1%AgOᵧ/SBA-15 catalyst. This suggests that the catalytic activity of composite metal oxides is higher than that of single component. In view of the reason, Wang et al. (2015) and Chen et al. (2011) found that the catalysts loaded with Ag could form stronger π-complex and had higher adsorption capacity for toluene, resulting remain time in the plasma system was increased. Ag could also weaken the Fe-O bond and increase the lattice oxygen mobility (Scirè et al., 2001). On the other hand, Ag reoxidation was readily accomplished by the transfer of adsorbed oxygen from FeOₓ, which could contribute to maintain the good performance for toluene degradation in the plasma system. These results indicate that the interaction between Ag and Fe species could increase the catalyst activity, and consequently improve the performance of the plasma-catalytic degradation of toluene.

**In Situ FT-IR Spectroscopy of Toluene Adsorption**

In situ FT-IR technology could provide continuous monitoring for VOCs adsorption over the catalyst surface (Augugliaro et al., 1999). Therefore, in situ FT-IR spectroscopy of toluene adsorption over the catalyst surface was carried out under the condition of 80% N₂ + 20% O₂ (Fig. 3). The band of the toluene adsorption appeared on all the catalysts: 1392, 1460, 1495 and 1608 cm⁻¹ characteristics of aromatic ring C=C stretching vibration (Li et al., 2007); 2879, 2928 cm⁻¹ characteristics of C-H vibrations of methyl (Maira et al., 2001; Eby et al., 2012); 3031 cm⁻¹ characteristic of C-H vibration of aromatic ring (Maira et al., 2001). Also, the new adsorption bands at 1120, assigned to terpene OH stretching (Das et al., 2014), and 1167, assigned to ester C-O stretching (Long et al., 2011; Yang et al., 2013), appeared on the surface of catalyst loaded with Ag. This indicates that the toluene oxidation on the catalyst surface was improved due to the Ag introduction. However, deep oxidization was not accomplished at room temperature, and as a result, it

![Fig. 2. Effect of catalyst on (A) toluene removal efficiency and (B) CO₂ selectivity (Initial concentration of toluene: 100 ppm, SED: 767 J L⁻¹).](image-url)
produced unexpected terpenoid and ester. There was no significant difference for the absorption band at 3616 cm$^{-1}$, characteristic ascribed to OH stretching (Li et al., 2011a, b), on the SBA-15 and 3%FeO$_x$/SBA-15, while this peak intensity increased on the surface of 2%FeO$_x$–1%AgO$_y$/SBA-15 catalyst. Those indicate that Ag incorporation could promote the generation of derivatives related to OH (Li et al., 2011b), which might be beneficial to toluene degradation on the surface of catalyst (Fig. 2).

**Analysis of the Toluene Oxidation Residues**

Byproducts on the catalyst surface were monitored by GC-MS (Fig. 4). The results show that the benzaldehyde, 4-methyl-2-pentanone had relatively high amounts on the SBA-15 surface, while they significantly decreased when Fe and Ag were introduced. This suggests that Fe and Ag loading could promote toluene oxidation in the process of NTP combined catalyst, which agreed with the results of CO$_2$ selectivity (Fig. 2).

**Catalyst Characterization**

In order to study the relationship between catalyst structure and toluene removal efficiency, the catalysts were characterized by XRD (Fig. 5), SEM (Fig. 6) and H$_2$-TPR (Fig. 7).

**XRD**

The results of low-angle XRD patterns (Fig. 5(a)) show the characteristic peaks, (100), (110), and (200), of mesoporous material and indicates that highly ordered 2D-hexagonal mesoporous structure of SBA-15 was retained after loading Fe and Ag. Fig. 5(b) shows the wide-angle XRD patterns of SBA-15, 3%FeO$_x$/SBA-15 and 2%FeO$_x$–1%AgO$_y$/SBA-15 catalysts. The Fe$_2$O$_3$ and Fe$_3$O$_4$ diffraction peaks were clearly observed when 3%Fe was loaded on SBA-15. However, they disappeared while Ag$_2$O and Ag diffraction peaks were observed as Ag species incorporation. This tendency might be caused by the formation of amorphous iron, or the fact that the particles of iron oxidation are highly dispersed on the support material with the such low amount Fe loading, resulting in the exceedance of detection limit with XRD.

Ag could serve as a reservoir for gas-phase toluene because of the π bond formation with toluene (Huang et al., 2015). Ag$^+$ is better at adsorbing toluene and weakening its C=C bond (Trinh et al., 2015; Qin et al., 2016). This could promote the toluene transformation from gas phase to the catalyst surface, then decrease the toluene degradation in the gas phase by the NTP, and improve the CO$_2$ selectivity during the toluene plasma-catalyst oxidation (Fig. 2). In addition, the Ag$^+$ on the catalyst is essential for high catalytic activity of CO oxidation (Zhang et al., 2013), which might be the reason for high CO$_2$ selectivity in the process of toluene degradation in the combined Ag-Fe NTP system.

**SEM**

The catalyst morphology was observed by SEM (Fig. 6). Some small granules appeared and evenly dispersed on the SBA-15 surface when the 3%Fe was loaded. However, the amount of particles decreased as 1%Ag incorporating, and the particles were smaller than those on the surface of 3%FeO$_x$/SBA-15. In order to study the morphology of the particles on the 2%FeO$_x$–1%AgO$_y$/SBA-15 surface, SEM of 2.5%FeO$_x$–0.5%AgO$_y$/SBA-15 and 1.5%FeO$_x$–1.5%AgO$_y$/SBA-15 were also provided (Figs. 6(d) and 6(e)). There were no large particles on the 2.5%FeO$_x$–0.5%AgO$_y$/SBA-15 catalyst, but some particles newly appeared on the 1.5%FeO$_x$–1.5%AgO$_y$/SBA-15 surface, and their size was even larger than those on the 3%FeO$_x$/SBA-15. This suggests that the particles on the 2%FeO$_x$–1%AgO$_y$/SBA-15 surface were the Ag compounds, and the diffusion of FeO$_x$ particles were promoted by Ag incorporating. These results might benefit for the improvement of FeO$_x$ catalytic activity.
The catalytic property of catalyst was determined by the reducibility, which could be measured by H$_2$-TPR (Gogoi et al., 2020). Fig. 7 presents the H$_2$-TPR profiles of different catalysts. The reduction peak at 126°C was observed in all catalysts and had no obvious change after Fe and Ag incorporation, which was attributed to the H$_2$ consumption by SBA-15. For the 3%FeO/SBA-15 catalyst, the low-temperature reduction peak (325°C) and a shoulder peak (438°C) could be attributed to the reduction of Fe$_2$O$_3$ → Fe$_3$O$_4$ → Fe (Long et al., 2011; Zhang et al., 2012a). In order to study the reduction of Ag, H$_2$-TPR profile of 3%AgO/SBA-15 was also carried out. Only one reduction peak could be observed at 110°C assigned to the reduction of Ag$^{+}$ to Ag (Chen et al., 2011), while it did not appear on others catalysts. Therefore, all the reduction peaks in the 2%FeO–1%AgO/SBA-15 could be assigned to the reduction of FeO$_x$. At the same time, all reduction peaks shifted to the lower temperature at the catalyst of 2%FeO–1%AgO/SBA-15 than 3%FeO/SBA-15. This suggests that the reducibility of FeO$_x$ was promoted, indicating that the lattice oxygen mobility was higher in 2%FeO–1%AgO/SBA-15 (Jin et al., 2013). Therefore, 2%FeO–1%AgO/SBA-15 catalyst showed the better performance for CO$_2$ selectivity in the plasma system (Fig. 2(b)).

**Pathways of Toluene Degradation**

Based on the results of toluene removal efficiency, analysis of organic byproducts, and in situ FT-IR spectroscopy of toluene adsorption, the mechanism of toluene degradation is proposed (Fig. 8). Toluene decomposition in plasma-assisted catalysis could be described to direct plasma reaction and plasma-catalytic surface reaction.

For the direct plasma reaction, it contains direct electron attack or indirect reactions between VOC molecules and gas-phase radicals. As we all know, there are a large number of high-energy electrons in the plasma system, which could react with O$_2$, H$_2$O and N$_2$ in the outlet gas as follows (R4–R10), and form gas-phase radicals (O$^·$, OH$^·$ and N$_2^*$) (Blin-Simian et al., 2009; Yu et al., 2010; Abdelaziz et al., 2013; Liang et al., 2013; Chung et al., 2019). The high-energy electron and the activity radical could induce the toluene degradation (ring opening, oxidation) in gas phase, and formed CO$_2$ and H$_2$O.
Fig. 6. SEM images of various catalysts. (A) SBA-15, (B) 3%FeO\textsubscript{x}/SBA-15, (C) 2%FeO\textsubscript{x}–1%AgO\textsubscript{y}/SBA-15, (D) 2.5%FeO\textsubscript{x}–0.5%AgO\textsubscript{y}/SBA-15, (E) 1.5%FeO\textsubscript{x}–1.5AgO\textsubscript{y}/SBA-15.

Fig. 7. H\textsubscript{2}-TPR profiles of different Fe and Ag loading catalysts (a: SBA-15, b: 3%FeO\textsubscript{x}/SBA-15, c: 2%FeO\textsubscript{x}–1%AgO\textsubscript{y}/SBA-15, d: 3%AgO\textsubscript{y}/SBA-15).

\[ e + O\textsubscript{2} \rightarrow e + O\cdot(\text{3P}) + O\cdot(\text{3P}) \]  
\[ e + O\textsubscript{2} \rightarrow e + O\cdot(\text{1D}) + O\cdot(\text{1D}) \]  
\[ e + H\textsubscript{2}O \rightarrow OH\cdot + H\cdot \]  
\[ e + H\textsubscript{2}O \rightarrow O\cdot + 2H\cdot \]  
\[ H\textsubscript{2}O + O\cdot(\text{1D}) \rightarrow 2OH\cdot \]  
\[ N\textsubscript{2} + e \rightarrow N\textsubscript{2}\cdot + e \]  
\[ N\textsubscript{2}\cdot + O\textsubscript{2} \rightarrow O(\text{3P}) + O(\text{3P}) + N\textsubscript{2} \]

When the SAB-15 was introduced into the plasma system, toluene could be adsorbed on the catalyst surface, and oxidized into the benzyaldehyde, then experienced through an opening of aromatic ring to form 4-methyl-2-pentanone, and further oxidized into CO\textsubscript{2} and H\textsubscript{2}O by O\cdot and •OH. As the
3%Fe was loaded on the SBA-15 surface, the O₂ in the gas phase could also be adsorbed on the catalyst surface via facile inter-conversion between Fe²⁺ and Fe³⁺ states, which could lead to the formation of free radical of O₂⁻. The generated O₂⁻ was then transported to the toluene on the catalyst surface, leading to a fast opening of its aromatic ring, and the further oxidation to CO₂ which finally desorbed from catalyst surface into gas phase. When Ag was incorporated, the amount of the OH was significantly improved (Fig. 3) because of the interaction between FeOₓ and AgOᵧ. As discussed above, a fast opening of the aromatic ring happened and led to the formation 4-methyl-2-pentanone, which then was mineralized to CO₂, and finally desorbed from catalyst surface into gas phase. On the other hand, toluene could also be adsorbed on the catalyst surface because of the π bond formation between Ag and toluene, then oxidized by oxygen from FeOₓ adsorbed, subsequently, mineralized into the CO₂ and H₂O. At the same time, Ag reoxidation was readily accomplished by the transfer of adsorbed oxygen from FeOₓ, Therefore, the reaction of toluene oxidation could be sustained. Meanwhile, the consumed oxygen species on the catalysts could be replenished by either gas-phase oxygen, or active oxygen species generated during the plasma process. The consumed oxygen in the gas phase would alleviate the effect of oxygen’s negative electrons on the process of toluene removal.

**Evaluation of Catalyst Stability**

The stability of SBA-15, 3%FeOₓ/SBA-15 and 2%FeOₓ–1%AgOᵧ/SBA-15 catalysts (Fig. 9), during toluene plasma-catalytic oxidation, was assessed at room temperature and atmospheric pressure. It was observed that toluene removal proceeded stably during the first 19 h for all the catalysts. After that, the toluene removal efficiency decreased in SBA-15 and 3%FeOₓ/SBA-15, while the 2%FeOₓ–1%AgOᵧ/SBA-15 catalyst was perfectly stabilized over the period of 37 h for toluene conversion. This suggests that the interaction between Ag and Fe improved the stability of catalyst.

Meanwhile, toluene removal efficiency shows the variation from 80% to 100% in SBA-15 and 3%FeOₓ/SBA-15, which might be due to an accumulation of water molecules on the catalyst surface (Lu et al., 2014). However, this phenomenon did not appear at the 2%FeOₓ–1%AgOᵧ/SBA-15 combined NTP system. This suggests that adding Ag improved the catalyst’s capability of resisting water molecules, which was very important to improve catalytic activity of the catalyst.

The XRD of the catalysts for different reaction times were compared to study structural stability of the catalysts (Fig. 10). Three characteristic peaks, (100), (110), and (200), characterizing the mesoporous material with 2D-hexagonal structure, were clearly identified, and no other diffraction peak was observed. This indicates that highly ordered 2D-hexagonal mesoporous structure of SBA-15 has not been altered by the plasma, although SBA-15 and 3%FeOₓ/SBA-15 had suffered slight deactivation during the toluene plasma-catalytic oxidation.
Fig. 9. Toluene removal over different catalysts as a function of time (Initial concentration of toluene: 100 ppm; feed gas: 80%N₂ + 20%O₂).

Fig. 10. The low-angle XRD patterns of different catalysts after reaction in plasma at 767 J L⁻¹.

CONCLUSIONS

Combining 3%FeOₓ/SBA-15 and 2%FeOₓ–1%AgOᵧ/SBA-15 catalysts with NTP drastically improved their toluene removal efficiency and CO₂ selectivity and markedly reduced the production of organic intermediates. Of these two catalysts, 2%FeOₓ–1%AgOᵧ/SBA-15 exhibited higher CO₂ selectivity and catalyst stability when introduced into nonthermal plasma, which was probably due to the reduced size and the increased dispersion and reducibility of the FeOₓ particles following the incorporation of Ag. In addition, Ag, existing in the form of Ag₂O and Ag particles on the catalyst surface, adsorbed toluene and promoted the production of hydroxyl groups, thus improving the reductive activity of the FeOₓ. These findings can be used to further optimize the use of FeOₓ and AgOᵧ in plasma-assisted catalyst systems for toluene degradation.

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REFERENCES


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